NASA Technical Memorandum 72866

AIFTDS STAND-ALONE RMDU FLIGHT TEST REPORT

(NASA-TM-72866) AIFTDS STAND-ALONE RMDU FLIGHT TEST REPORT (NASA) 63 P HC A04/MF A01 CSCL 01C

N79-28167

Unclas G3/05 29450

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July 1979





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1.0 INTRODUCTION

The Airborne Integrated Flight Test Data System (AIFTDS) developed by NASA Dryden through contracts NAS4-1848 and NAS4-2161 has been subjected to two analytical studies in the past two years. The first study was designed to indicate the accuracy and operational characteristics in a hostile laboratory environment and was concluded with the publication of NASA TMX-56043. This report covers work, which commenced in mid-1976 and concluded with the last flight in July, 1977, and was designed to identify the AIFTDS performance characteristics in an actual flight environment.

1.1 Background on AIFTDS Stand-Alone Flight Test

Several documents and articles, published by both NASA and private industry, discuss the AIFTDS concept in its entirety; however, no document exists to date which analyzes the AIFTDS in a flight environment. NASA Dryden does not routinely evaluate electronic data acquisition systems in a flight environment; however, it was judged appropriate to do so for the AIFTDS. The reasoning for the decision was two-fold: first, the AIFTDS is an extremely complex, but flexible, pulse code modulation (PCM) system which requires considerable user familiarity for effective application. Second, it was deemed necessary to provide a baseline for future reference when the AIFTDS is in widespread use at Dryden Flight Research Center.

In conjunction with the two reasons stated above were the objectives of the flight test:

- a. To familiarize the Dryden crew with the AIFTDS hardware and operation characteristics.
- b. To study the accuracy and resolution of the system in a flight environment.
- c. To determine shielding and instrumentation techniques for a system as sensitive as AIFTDS.
- d. To obtain hard-copy PCM data from the flights through the Center's data reduction system.

Dryden's Measurement Engineering Branch proceeded with the flight test of the AIFTDS in 1976.

1.2 Discussion of Flight Test Plan

Because the AIFTDS is, as the name implies, a PCM data acquisition <u>system</u>, a flight test plan was formulated which divided the task into two phases. One phase was the flight test of the stand-alone remote multiplexer/digitizer unit (RMDU), while the second phase will be the flight test of the RMDU in conjunction with an airborne computer, an RMDU Controller Unit (RCU), and a Cockpit Control/Display Unit (CCDU), see Figure 1. This report covers only the first phase.

The knowledge gained through the first phase of the flight test will be applied directly to the as yet uncompleted second phase; e.g., optimum RMDU wiring configurations as well as sensor instrumentation developed in phase one are extremely important in the configuration control of the second phase of the flight test.

2.0 BACKGROUND ON AIFTDS

2.1 <u>Background on the Dryden Stand-Alone Remote Multipler/Digitizer</u> Unit (RMDU)

NASA Dryden's stand-alone configured RMDU used in the flight test program utilized the following plug in modules and/or cards: analog multiplexer (AMX) cards, presample filter/amplifier (PSF) card, excitation/bridge completion (EBC) card, analog data processor module (ADP-M), and the standalone timing module (SAT-M) see Figures 2a through 2e. A brief description of each is presented in Appendix 1.

2.2 Symbols and Abbreviations List

| ADP-M | Analog Data Processor Module |
|---------------|---|
| AIFTDS | Airborne Integrated Flight Test Data System |
| ALT | Approach and Landing Test |
| AMX | Analog Multiplexer |
| AC.1 - AC.4 | Accelerometer #1 - Accelerometer #4 |
| BiØ−L | Bi-phase Level |
| BiØ-M | Bi-phase Mark |
| CPT 1 - CPT 4 | Control Position Transducer #1 - Control Position Transducer #4 |
| DC | Direct Current |
| DM-M | Delay Modulation Mark |
| EBC | Excitation/Bridge Completion |
| EPROM | Eraseable Programmable Read Only Memory |
| GPA-Ø | Gain Programmable Amplifier's Zero Input Response |
| HLC | High Level Calibration |

ILT/Premod Filter Isolation Line Terminator/Premodulation

Filter Unit

ips Inches per second

IRIG Inter Range Instrumentation Group

LFC Laminar Flow Control

LLC Low Level Calibration

LSB Least Significant Bit

MSB Most Significant Bit

MSBLS Microwave Scanning Beam Landing System

NRZ-L Non-Return to Zero Level

NRZ-M Non-Return to Zero Mark

PCM Pulse Code Modulation

PSB Power Supply Bite (Built In Test Equipment)

PSF Presample, Amplifier Filter

PT1 - PT4 Pressure Transducer #1 - Pressure Transder

#4

RCU- RMDU Controller Unit

RMDU Remote Multiplxer/Digitizer Unit

SAT-M Stand-Alone Timing Module

TC Thermocouple

TM Telemetry

W.O.L. Wallace O. Leonard

2.3 Flight Test Background

Normally, a flight test program of this scope would require a period of from 6 months to a year to accomplish. The flight testing of Dryden's

stand-alone system took approximately 19 months of which 9 months were actually devoted to flights. Several factors contributed to this time lag:

- a. The Center viewed the AIFTDS as a low priority project.
- b. The parameters originally requested had been wired in the aircraft (aircraft used was a modified Lockheed Jetstar see Figure 3) circa 1970, and proved to be highly unreliable due to shielding and connector problems.
- c. Project engineer and project instrumentation engineer were changed during the tests.
- d. Higher priority programs (MSBLS, LFC, etc.) instituted after the start of the AIFTDS flight test program severely impacted the work schedule.
- e. Time onboard the aircraft was restricted because of reason #4: "wringing out" or verification of the existing system was virtually impossible as was the opportunity to install new sensors in the aircraft.
 - f. Software was not available to analyze data on ground station.

The original parameter list agreed upon by the AIFTDS project engineer in 1975 included the following parameters, for which wiring was reported to be installed on the aircraft:

Early Jetstar Parameter List

Control Position Transducers: (Hi-Level Outputs)

- (1) Throttle Position
- (2) Rudder Pedal Position
- (3) Rudder Position
- (4) Aileron Position
- (5) Elevator Position
- (6&7) Stabilizer Position
- (8) Alpha Vane

Nose Boom

(9) Beta - Vane

Accelerometers:

- (10) Lateral CG Acceleration
- (11) Longitudinal CG Acceleration

- (12) Right Hand Horizontal Stabilizer Root Leading Edge Vertical Acceleration.
- (13) Right Hand Horizontal Stabilizer Root Trailing Edge Vertical Acceleration.
- (14-17) Tail Accelerometers #1, #3, #4, #5 Hi-Level Output
- (18&19) Tail accelerometers #6, #7 Low Level Output

Pressure:

- (20) Air Speed Coarse
 (21) Air Speed Fine

 0 750 PSFA W.O.L.
- (22) Altitude Coarse (23) Altitude Fine $\begin{cases} 0 - 2200 \text{ PSFA W.O.L.} \end{cases}$
- (24) Rudder Pedal Force
- (25) Rudder Differential Pressure
- (26) Aileron Wheel Force
- (27) Total Reference Pressure
- (28) Elevator Differential Pressure

Gyros:

- (29) Roll Rate
- (30) Yaw Rate

Presicison Voltages:

(31-42) Precision Voltages from Divider Box.

A pacer flight to calibrate the Jetstar's airspeed indicators with a calibrated craft was scheduled for June 3, 1976. This flight revealed that only 4 sensors of the 30 requested were operating. Six weeks later on July 14, another flight was flown. By this time 9 of the original 42 parameters had been installed and checked out. Two days later on July 16, another checkout flight was made; 8 sensors were operational, 14 precision voltages were employed, and 17 of the disabled sensor channels were shorted at the pallet. This flight was the first flight in which data was directed through the ground station. It then became painfully obvious that an excessive amount of time would be needed to insure the correct installation of the original sensors which were requested.

3.0 STAND-ALONE FLIGHT TEST

3.1 The AIFTDS Experimental Sensor Box Concept

It was also during this time frame (May-July 1976) when the Approach and Landing Testing (ALT - for the Shuttle program) was beginning to become active. The Jetstar was chosen as the test bed for the ALT Microwave Scanning Beam Landing System (MSBLS) as well as the facility for the Laminar Flow Control (LFC) project. The AIFTDS project had the lowest priority and hence, very little work was carried out on the Jetstar to satisfy the sensor configuration requirements.

It was at this time when the AIFTDS project leader decided to abandon the original idea of using the ship's sensors for the flight test phase. A plan was formulated which would benefit the project in two ways:

- a. Trade time in the lab for actual time on the aircraft for wiring and testing of the system.
- b. Would give the AIFTDS project leader complete control over sensor wiring configurations and shielding and excitation designs.

A sensor housing box was designed and constructed (See Figure 4) which was mounted inside the aircraft and fulfilled the original requirements of the AIFTDS flight test phase. In this box was a selection of commonly used sensors; i.e., strain gages, thermocouples, control position transducers (CPT's), accelerometers, and resistors. Four similar strain gages, four similar accelerometers, and four similar CPT's, as well as two similar TC's and two similar resistors were chosen. For the strain gages, accelerometers, and CPT's, there were four different methods of installation as follows:

- (1) Sensor excited by an integrated signal conditioning card, and having the shield referenced or driven at the sensor end.
- (2) Sensor excited by integrated signal conditioning and grounding the shield at the RMDU.
- (3) Sensor excited by DFRC "standard" external signal conditioning boxes, and having the shield referenced at the sensor end.
- (4) Sensor excited externally with the shield grounded at the RMDU.

For the thermocouples and the resistors the configurations were limited to shield referencing either at the sensor end or at the RMDU end (see Figures 5 and 6). With the design and construction of this sensor box, the priority/time conflict on the Jetstar and configuration control problems were resolved. On the final two flights (June-July 1977) an active pre-sample filter was employed with four of the sixteen sensors. The results from the filtered data was compared with the unfiltered responses of previous flights.

3.2 Jetstar Flight Schedules

As mentioned previously, several higher priority projects began using the aircraft originally chosen for the AIFTDS. Such additional projects, Microwave Scanning Beam Landing System (MSBLS) - part of the Shuttle Approach and Landing Tests, the Laminar Flow Control project and others, created an added burden on the flight scheduling. The MSBLS project needed a large number of flights to effectively checkout the landing system - sometimes multiple flights per day. This, of course, meant that any AIFTDS work on the aircraft had to be completed between pre-flight checks. This constraint also dictated the flight plan for the AIFTDS project when both AIFTDS and MSBLS were flown together. The Laminar Flow Control Experiment (LFC) required lengthy flights (> 90 minutes) to achieve its purpose.

The length of the LFC flights created two major problems: extending the use of the onboard tape recorder for the entire flight, and causing telemetry link dropouts by the extreme range involved. An additional problem of scheduling these flights was the time sharing of the instrumentation pallet for the multiple projects, the tape recorder and transmitter. Cooperation between the various projects was a must in order to satisfy both data requirements.

During the peak months of activity on the Jetstar as many as 4 or 5 flights were being scheduled weekly - any last minute cancellation or alteration of the flight schedule or plan would require additional manpower support from the telemetry ground station. Conflicts with the TM ground station coverage due to these cancellations or alterations often acted to eliminate the telemetry down link coverage of the AIFTDS PCM data. This, in effect, resulted in poor data visibility since no data could be verified until the ground station could play back the airborne record tape at a later date. Nonetheless, with all of these flight scheduling proglems, the AIFTDS project received the requested six data flights in a 9 month period.

3.3 Discussion of AIFTDS Data Acquisition Procedure and Equipment

A block diagram of the AIFTDS data acquisition system utilizing the AIFTDS Experimental Sensor Box as sensor input, is shown in Figure 7. A photograph of the instrumentation pallet is shown in Figure 8.

The AIFTDS Experimental Sensor Box schematic and photograph is shown in Figures 4, 5, and 6. From the schematic it can be seen that sensors PT3, PT4, AC.3, AC.4, CPT3, and CPT4 have their power derived from the pallet external signal conditioning unit. It can also be seen that sensors PT1, PT2, AC.1, AC.2, CPT.1, and CPT.2 obtain power through either the RMDU internal signal conditioning card (EBC card) or through the RMDU power supply itself. All sensors in the AIFTDS Experimental Sensor Box, however, receive their stimuli from the box itself; each individual group of sensors is exposed to identical stimuli. This factor, in conjunction with the fact that the individual group of sensors are identical allows the investigator to accurately compare data responses for the four excitation and shielding combinations.

The responses from the 16 sensors in the AIFTDS Experimental Sensor Box along with some internal RMDU "health check" signals (LLC for gains of 1000, 400, 100; HLC, GPA-Ø for gains of 400, 10; and PSB) and some shorted channels were processed and digitized by the RMDU. The RMDU has the capability of simultaneously generating two serial PCM bit streams in different codes for routing to different post-processing media. The output coding formats available are: NRZ-L, M; BiØ_L,M; and DM-M. The output data stream being sent to the onboard tape recorder is in the format of DM-M (for improved low frequency response and minimum DC base line drift) while the data stream being sent to the transmitter is in NRZ-L format. The use of these two formats is standard at NASA Dryden.

The DM-M formatted PCM data stream is recorded on the Model AR-700 airborne tape recorder in the direct mode. The NRZ-L formatted PCM data stream sent to the transmitter is first directed to a premodulation filter having a cutoff frequency of 160 Kbits/sec. The filtered output is then used to frequency modulate the telemetry transmitter carrier of 1521.5 MHz. See Figures 9 and 10 for the circuit schematic and connector configuration, and the photograph in Figure 11 for a detailed view of the filter box.

A crucial part of the AIFTDS flight test was the use of the onboard flight test engineer. The flight test engineer recorded flight data by hand through the use of the flight line tester which was mounted on the instrumentation pallet. The flight line tester, being a portable PCM decommutator, allowed the flight test engineer to record data from any of the parameters during the flight to be compared with the data processed on the ground station.

3.3.1 Real Time Processing of PCM Data

The 1521.5 MHz telemetry signal is received at the Dryden telemetry ground station. For the AIFTDS flights the PCM stream was received by the series 410 receivers and then processed by the decommutation equipment. The decommutation equipment (consisting of EMR Model 720 PCM bit synchronizer, Model 2731 PCM frame synchronizer, and Model 2736 PCM subframe synchronizer) is programmed and controlled by the SEL (Systems Engineering Laboratory) Model 86 and 810B computers.

Through this interaction between the SEL computer and the decommutation equipment, certain parameters were selected for real time display. The real time display was 32 tracks of stripchart recording in the high range ground station control room. In addition to the 32 displayed parameters, the IRIG timing track from the ground station was also displayed. IRIG-B time code generators are used to establish time correlation between real time data and that data which is recorded on the onboard tape recorder. Because of computer input/output limitations the stripchart outputs represent samples at a maximum rate of 5ms/sample (200 samples/Sec - which is the rate of the PCM system currently in use at Dryden).

3.3.2 <u>Telemetry Dropouts</u>

Even with directional tracking antennas the maximum range attainable with approximately 5 watts of power at 1521 MHz into the blade transmitting antenna on the aircraft is 200-300 miles (320 Km-480 Km) taking into account propogation and the aircraft's altitude. Anything between the aircraft and the receiving antenna (over the horizon, mountains, buildings, etc) severely limits this maximum range. In fact, the only reliable reception is limited to line of sight ranges. Any distance greater than this or any obstacles between the aircraft and the receiving antenna can (and usually will) cause telemetry dropout. TM dropouts can cause the PCM decommutation equipment to lose synchronization and, hence, cause "noise" to appear at the output and on the stripcharts.

If the TM dropouts are of short duration the effect is transient irregularities on the stripchart outputs. These irregularities caused by TM dropouts interfere with the monitoring of the real time processed PCM data (in that the unadulterated data looks similar to that data which is contaminate by transient type noise). To examine the TM data during the times when dropouts occur is impossible and requires the onboard tape to be played back later to fill in data for dropout times.

The instrumentation pallet (which holds the entire data acquisition system for the project - see Figure 8) was shared with other ongoing experiments at this time (MSBLS, LFC, and others). During those portions of the flight when data was to be collected for the other project(s) the AIFTDS PCM bit stream was disconnected from the transmitter's modulation input. This effected a TM dropout, also which could extend for long periods of time. However, the onboard tape recorder was used for the collection of data during this time.

In the section of this report dealing with the analysis of the flight data, many dropouts are indicated by simultaneous loss of data on all channels (see appendix).

3.3.3 PCM On Board Recording

Onboard recording of the PCM data was accomplished using an airborne AR-700 Model tape recorder. On all AIFTDS flights the tape speed was 15 ips (250 KHz bandwidth) thus giving approximately 90 minutes of recording time. The coding of the PCM data for the tape recorder was in DM-M (Delay Modulation-Mark), as well as NRZ-L (non-return to zero level), and the recorder was operated in the "direct" record mode. The bit packing density of the tape did not exceed 12,000 bits/inch throughout the flight test.

The AR-700 is a 14 track recorder (when using 1 inch width tape); AIFTDS data (NRZ-L and DM-M formats) was recorded serially on two tracks. The IRIG-B time code generator signal was recorded on another track, with the remaining eleven tracks being devoted to functions relating to the other projects which were sharing the pallet.

The tapes from the onboard recorder were held until time was available for post flight processing. The time delay was governed by the ongoing progress towards developing the software package necessary to process the flight data and the work load in the telemetry facility at Dryden. The plan of attack for processing the flight data was as follows: The data which was manually recorded (via the onboard AIFTDS flight test engineer) was correlated with the real time strip chart data. The IRIG-B time was noted for any data of interest and that time was used for selecting that portion of the flight data tape for processing through the ground station computer. See Appendix 3 for samples of data reduction in this manner.

4.0 SUMMARY AND DISCUSSIONS

4.1 Flight Objectives and Achievements

A measure of a flight test project success is to compare the results with the goals and determine if the achieved results satisfied these goals. Recalling the goals from Section 1, each will be compared with the associated results.

4.1.1 Goal #1: Familiarize the Dryden Crew with the AIFTDS Hardware and Operational Characteristics

Throughout the flight test phase of the Stand-alone AIFTDS numberous people came into intimate contact with the AIFTDS.

- a. The instrumentation crew involved with the wiring and checking out of the AIFTDS installation.
- b. The personnel in the telemetry ground station responsible for the decommutation and processing of the real time data from the PCM telemetry link.
- c. The project engineers and the project managers involved with the overall planning and direction of the project.
- d. The persons involved with procurement and contract management were all involved with and familiarized with the AIFTDS hardware and/or the operational characteristics.

Although this goal was easily achieved, it would obviously be more effective if more people could have been trained and familiarized. However, not until the AIFTDS is in widespread use at the Center as its primary data acquisition system will all of the appropriate persons be familiarized with the AIFTDS system.

4.1.2 <u>Goal #2: To Determine Shielding and Instrumentation</u> <u>Techniques</u>

As was previously stated, the Dryden RMDU possesses a resolution of 12 bits; at a gain of 1000 each count represents 5 μ volts which is six times more sensitive than the existing systems presently in use at DFRC. In order to utilize this extreme sensitivity extra care must be exercised in the sensor wiring. It was shown early in the flight test program that the existing wiring and instrumentation (excitation and signal conditioning) of the Jetstar sensors was not adequate to make full use of this increased capability. Millivolt level noise (common mode and differential mode) destroys data validity when microvolt level measurements are desired.

The experimental sensor box data clearly demonstrates the trade-offs between excitation, signal conditioning, and shielding schemes (see Appendix 3). The best overall configuration of the sensors was to ground the shield at the sensor (to minimize common mode effects) and to utilize internal signal conditioning/excitation. This fact should not be too surprising to instrumentation engineers, however, the data from the flight test demonstrates this fact beyond any shadow of doubt.

In the process of determining the appropriate shielding and excitation techniques to use, care was exercised in not eliminating noise through the use of pre-sample filtering. This method of "cleaning up" the data can give false data in the area of shielding techniques. The AIFTDS was designed with increased flexibility so that pre-sample filtering is not needed in all cases. The need for filtering can sometimes be eliminated by increasing the sample rate. However, in cases where it is not possible or feasible to increase the sample rate (due to ground station limitations, tape recorder limitations, or any other reasons) the AIFTDS does have provisions for internal active-presample filter modules. As noted earlier in this report the presample filter used in the Dryden program was programmed for a gain of 400 on 3 of the 4 channels and a gain of 1 on one channel. The filters in all 4 cases were 4-pole Butterworth low pass filters having a cutoff frequency of This presample filter module was used on a select few parameters during the last 2 flights; comparison between filtered data and non-filtered data is made in the Appendix section.

4.1.3 Goal #3: To Obtain Hard Copy PCM Flight Data Through the Ground Station Facility

This goal was one of the most difficult to achieve: it certainly required the most time of all to achieve. The Dryden PCM processing system is a complex system consisting of two SEL 32 bit computers controlling the PCM decommutators. with an SEL 86 (central processing system, a Control Data Corp. Cyber Model 7328 control computer facility, as well as many software operating systems. This processing system, being large and complex, is very difficult to change or modify. Since the AIFTDS PCM format was different for this test phase from the systems currently in use at Dryden, a modification to the presen Dryden PCM processing scheme was necessary in order to process AIFTDS data. Of course, the modifications and additions to the processing system required programming manpower; with the onslaught of the Shuttle ALT program, as well as higher priority projects at the Center very little manpower was available to work on AIFTDS requirements. Consequently, the hard copy data was received from the ground station 6 months after the last flight.

Normally, a flight project request for data processing requires pre and post-flight calibration data in order to perform the polynomial fit to the data as well as to convert the data to engineering units. The data processing also usually involves data compression by the computer controlled decommutators in the ground station. However, the requirements for the AIFTDS PCM data processing were extremely rudimentary, e.g., the only desired output from the processing was a straight decimal conversion of the raw offset binary data. In addition to the binary to decimal conversion, the display of stripchart data correlated with the IRIG-B time and the word frame and/or subframe number was requested. Data compression or engineering conversions were not performed on this data, however the gain tag bit conversion was accomplished (the gain tag bit has been discussed earlier) when converting the offset binary data to decimal value.

Because of the minimal requests for PCM data processing levied on the data reduction personnel, all the requested functional capabilities were provided in the telemetry ground station facility. This completely eliminated the need for Cyber system software and operational manpower. The PCM hard copy data was handled in a manner similar to that of the real-time strip chart outputs. The front end telemetry hardware (bit, frame, and subframe synchronizers) decommutated the flight data under control of the computer.

The flight data recording tape was played back at 1/4 speed so that the data sample rate would not exceed the output hardware I/Ø capabilities of the existing system software and hardware. Data then was provided at 5ms intervals (corresponding to Dryden's 200 samples per second existing data acquisition systems) on a hard copy line printer (see Appendix 3).

Flight data which was taken by hand in the aircraft was IRIG-B time correlated with that data which was displayed on the real time strip charts. Key time increments were then requested for the hard copy output. The hard copy PCM data was compared with that data obtained by hand and with that obtained from the real time strip charts in Appendix 3. From the examples illustrated in Appendix 3 it can be seen that the hand recorded data and the hard copy printout data correlate very closely with each other (±6 counts deviation). The strip chart data probably is also as accurate, however, the scale factor necessitates much coarser readings.

4.1.4 Goal #4: Study of Accuracy and Resolution of the AIFTDS System in a Flight Environment

Since hard copy PCM data has been made available to the AIFTDS team only recently, a complete analysis on the flight data may not be completed for some time. However, some accuracy and resolution analysis has been performed on some of the precision voltage inputs.

For these precision voltage input channels, several hundred samples were statistically analyzed. The occurrence of data values greater than 5 counts away from the norm were noted (see Appendix 3). Data point deviations on the order of 2 or 3 counts (for channels without presample filtering) were considered to be caused by instrumentation noise and/or thermal noise. From the analysis performed on these data it was determined that a deviation of 5 counts or more occurred less than once every 850 data values. For the most part, these large deviations were on the order of several hundred counts from the normal. The source of these large excursions has yet to be determined, although several possibilities have been brought to light. Instrumentation anomalies as well as anomalies in the ground station hardware are thought to be the most probable causes.

Appendix 3 illustrates several examples of precision voltage data. It is doubtful that the flight environment had any detrimental effects on the data validity save for an occasional noise anomaly. It is also obvious that the system can be made more immune to the aircraft noise environment with sound instrumentation engineering practices.

4.2 Impact of 12 Bit PCM Systems in Today's Aerospace Environment

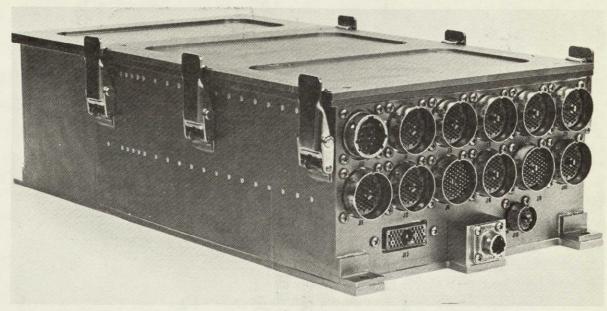
NASA Dryden Flight Research Center's experience in high resolution data acquisition systems took a major step forward in the mid 1960's with the advent of a 9 bit PCM system. This PCM system, called the CT-77, has served as the backbone of Dryden Flight Research Center's data acquisition systems. With the recent breakthroughs in hybrid analog

circuitry, PCM systems with resolutions in excess of 10 bits have been finding their way into the instrumentation engineer's arsenal. However, it is too soon to tell what effect, if any, this increase in resolution will have on PCM data acquisition systems.

One major advantage of a higher resolution, higher bit PCM data acquisition system (say 12 bits) over a 9 bit system is the increase in usable dynamic range available in the 12 bit system. Thus, by allowing each count to represent the same level there will be nearly one decade of range increase in the 12 bit system over the 9 bit system. This obviously allows for greater simplicity in data reduction (engineering units conversion, etc.) as well as allows for more leeway in the original estimation of output signal levels.

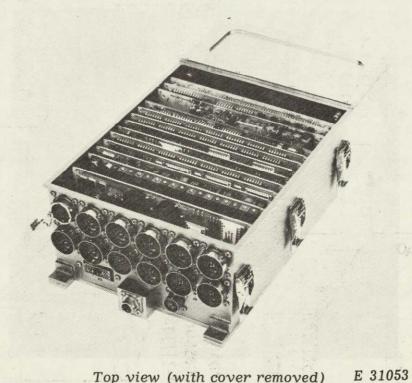
Another advantage is the obvious increase in sensitivity for the same dynamic full scale range. The same full scale range for a 12 bit system will allow an 8:1 increase in gain or resolution of each count over the 9 bit system. This advantage, however, also creates its own problems, e.g., the instrumentation engineer must properly shield and condition the transducers. Shielding and signal conditioning of transducers must be adequate to minimize common mode, differential mode, and ground loop coupling and other sources of data contamination. Since, in the case of aircraft instrumentation, there are usually many sensors located at remote locations referenced to the airframe potential in some manner, it is nearly impossible to eliminate one or all of these sources of error. This has a tendency to offset the advantages gained in the increased sensitivity (resolution per count) of the larger word size. There are, today, several groups of instrumentation engineers using the AIFTDS system with its increased word size and flexibility. NASA Ames, Douglas Aircraft Company, ERDA, and U.S. Air Force, to name only a few, have compiled many hours use with these systems - including many hours in a flight environment. Their experiences using the AIFTDS are well documented.

At NASA Dryden there are projects requiring accuracies on the order of 1/2% or better. These increases in accuracy requirements can be achieved easier with longer bit words; the quantizing error alone in an 8 bit system is on the order of .4% whereas it is only .025% in a 12 bit system. Hence, it is inevitable that the word length will have to increase if the dynamic range requirement or the accuracy requirement is to be satisfied. The penalties for this increase in word length are the increased care and engineering which must be exercised in instrumenting the newer system as well as the moderate increase in bandwidth required to keep the same word rate. The trade-offs are real and will have to be evaluated individually for each application.



Front View

Figure 1. AIFTDS standalone RMDU.



Top view (with cover removed)

Figure 1. Full AIFTDS system.



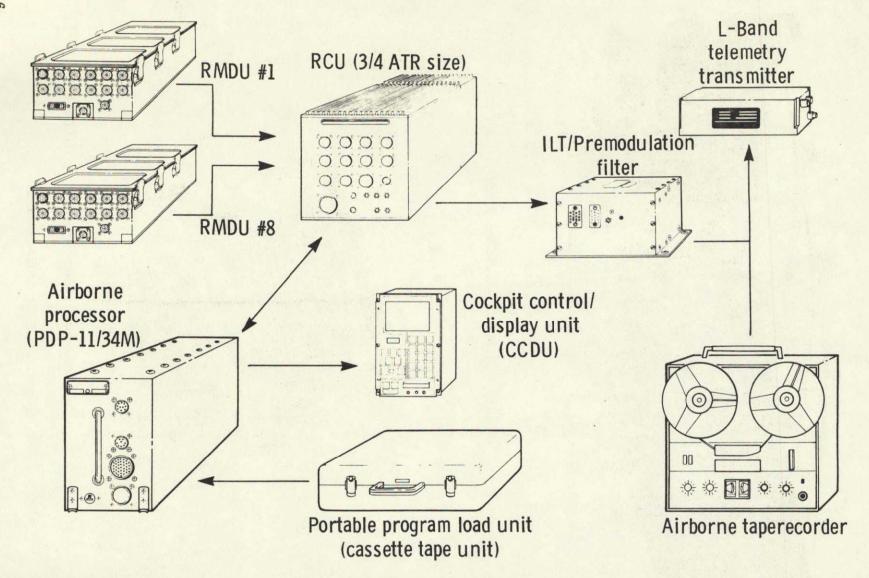
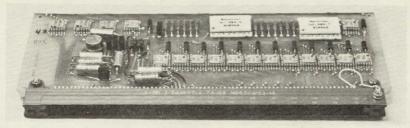
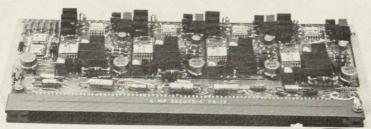


Figure 1. Full AIFTDS system.



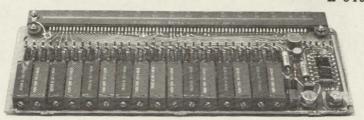
(a) Analog muliplexer (AMX) card.

E 34078



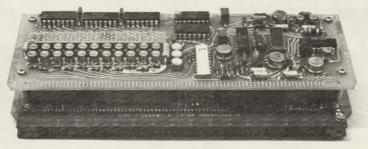
(b) Presample filter/ amplifier (PSF) card.

E 34077



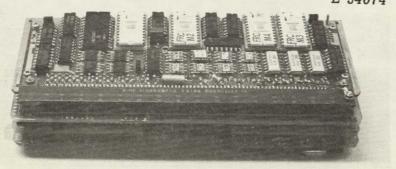
(c) Excitation/bridge completion (EBC) card.

E 34075



(d) Analog data processor module (ADP-M).

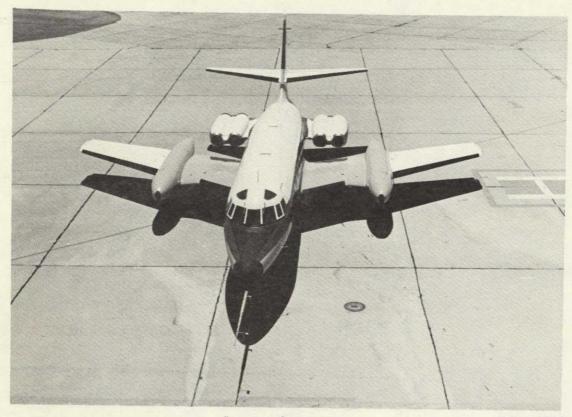
E 34074



(e) Stand-alone timing module (SAT-M).

E 34073

Figure 2. RMDU plug-in modules.



Jetstar front view

ECN 4039

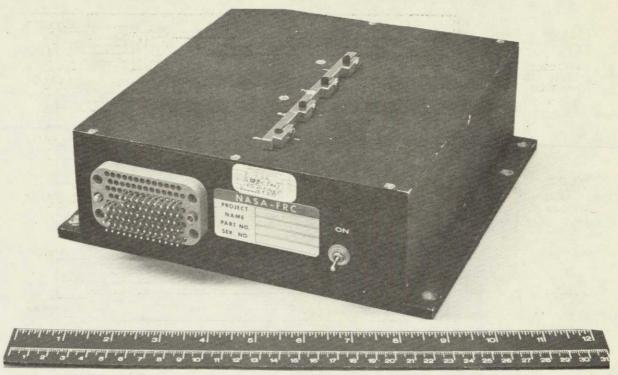


Jetstar side view

ECN 2401

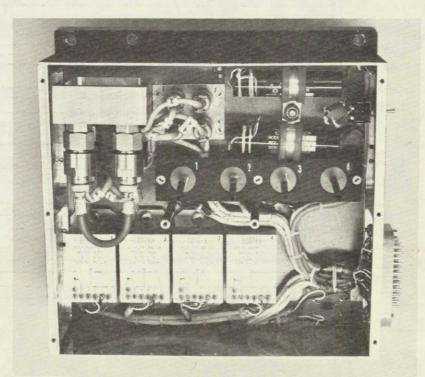
Figure 3. Jetstar.

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Experimental sensor box with cover plate in place

E 34082



Experimental sensor box with cover plate removed

Figure 4. Experimental sensor box.

E 34081

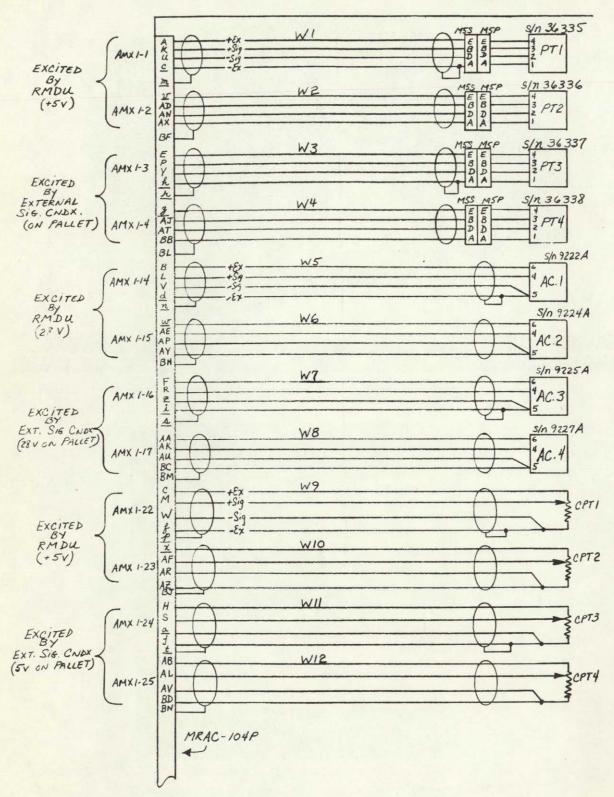
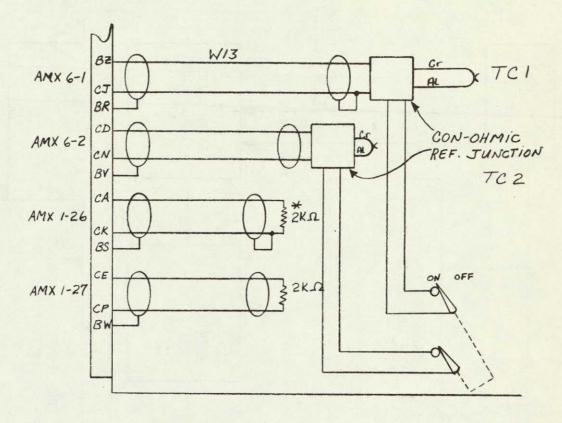


Figure 5. AIFTDS experimental box schematic (top section).



```
PTI: STATHAM PMI3ITC-20D-350; 20 psiD; 5V; S/n 36335
PT2 :
                                            S/n 36336
PT3 :
                                            S/n 36337
PT4:
                                            S/n 36338
AC.1: Donner; 28v; 10 & max; .4v/6; 5/N 9222A
                                    ; S/N 9224A
AC.2
AC.3
                                    ; S/N 9225A
AC.4
                                      S/N 9227A
CPTI-CPT4: 2KA HELIPOT
TCI: Chromel- Allumel 21/2 por/oF
TC2:
ZKAX: ZKA; 18W, . 1% Wire wound
2K1 :
```

Figure 6. AIFTDS experimental box schematic (bottom section).

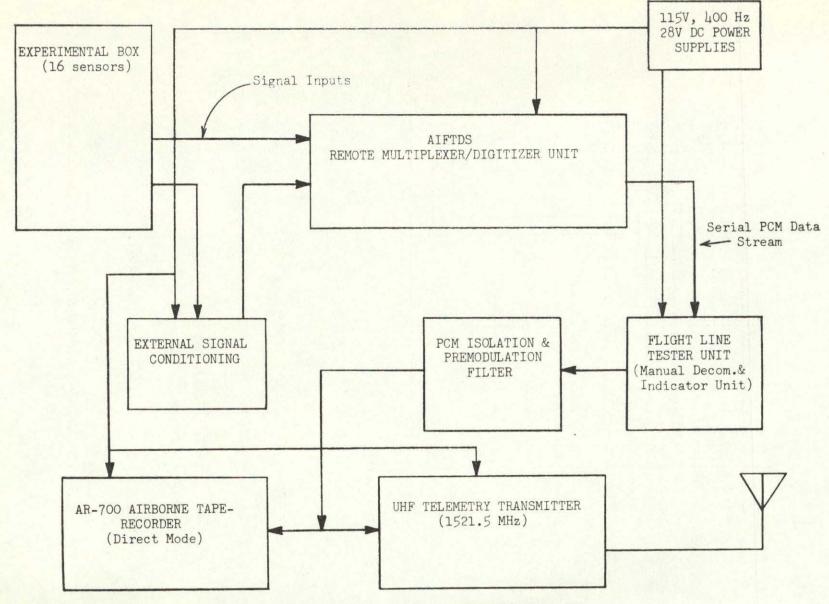


Figure 7. AIFTDS data acquisition system block diagram.

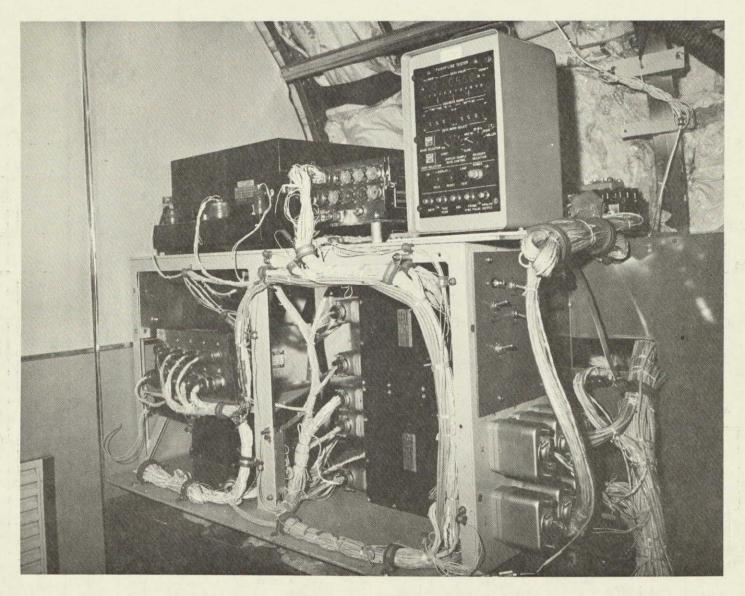


Figure 8. Instrumentation pallet.

E 30828

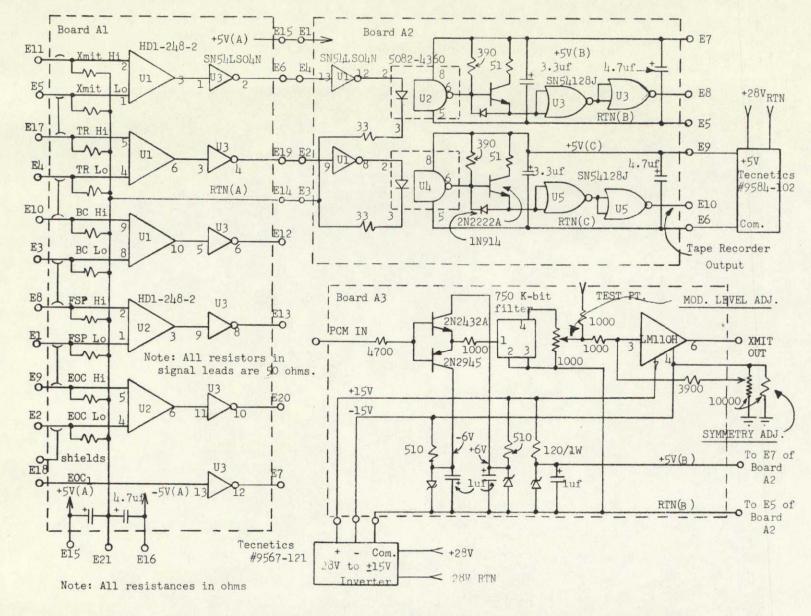
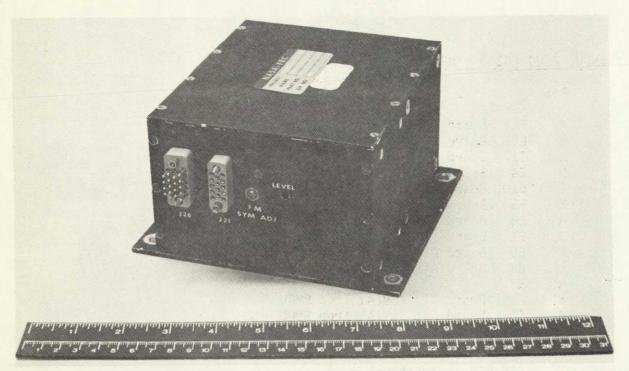


Figure 9. Schematic diagram of ILT/premodulation filter circuit.

INPUT PLUG (J20): MRAC-18P

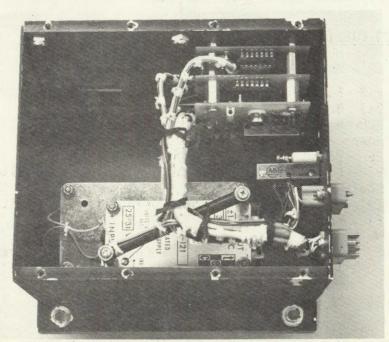
```
Destination
    Pin #
         Ell Board Al; XMIT Hi
               Board Al; XMIT Lo
    B
         E5
    C
          E17 Board A1; TAPE RECORDER Hi
    D
               Board Al; TAPE RECORDER Lo
    E
          E10 Board A1; BINARY CLOCK Hi
    F
               Board A1; BINARY CLOCK Lo
          E3
    H
          E8
               Board Al; FRAME SYNC PULSE Hi
    J
          E1
               Board A1; FRAME SYNC PULSE Lo
     K
          E9
               Board Al; END OF CYCLE Hi
               Board A1; END OF CYCLE Lo
     L
          E2
    M
          N2
     N
          E15 Board A1; +5V(A) from RMDU
          E16 Board A1; -5V(A) from RMDU
          E18 Board A1; EOC, TTL level signal from RMDU
     R
     S
          +28V to inverters
     T
          28V RTN to inverters
     U
          Shields |
     V
          E14 Board A1; RTN(A) from RMDU
OUTPUT PLUG (J21): MRAC-14S
               Board Al; ECC<sub>1</sub> TTL level signal
     A
          E7
     B
          E12 Board A1; BINARY CLOCK TTL level
          E13 Board A1; FRAME SYNC PULSE TTL level
          E20 Board A1; END OF CYCLE TTL level
     D
          Board A3; XMIT OUT RTN
               Board A2; TAPE RECORD OUT RTN
          E6
               Board A2; +5V(B) to be used only as a monitor point
          E7
     J
          Board A3; XMIT OUT Hi
     K
               Board A2; +5V(C) to be used only as a monitor point
          E10 Board A2; TAPE RECORD OUT Hi
          NC
          E7
               Board A1; RTN(A) from RMDU to be used as reference with pins
     N
               A,B,C,D
     P
          NC
     R
          NC
```

Figure 10. ILT/premodulation filter internal wiring schematic.



ILT/premodulation filter box with cover plate in place

E 34083



ILT/premodulation filter box with cover plate removed E 34080

Figure 11. ILT/premodulation filter box.

| | | | | · · · · - | | | | | | | | |
|-------|----|----|---|-----------|---|---|---|---|---|---|---|---|
| Bit # | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |

Format:

MSB

LSB

Note:

The MSB (Most Significant Bit) is the Gain Tag bit; when MSB = 0 the gain that was programmed is used, when MSB = 1 the programmed gain is reduced by $\frac{1}{2}$ through the auto-ranging amplifier circuit. The MSB is transmitted first.

The remaining 11 bits are in offset binary format.

Examples:

Decimal Equivalent Translation

| | MS | В | | | | · | | | | | | | LSB |
|--------------|----|---|---|---|---|---|-------------|---|---|---|----|---|-------------------------------|
| -1024* | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ٠0 | 0 | $(0-1024) \times 2 = -2048$ |
| -768* | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(256-1024) \times 2 = -1536$ |
| -633* | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | $(391-1024) \times 2 = -1266$ |
| -512 | 0 | 0 | 1 | 0 | 0 | 0 | ۰0 | 0 | 0 | 0 | 0 | 0 | $(512-1024) \times 1 = -512$ |
| -256 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(768-1024) \times 1 = -256$ |
| -64 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | $(960-1024) \times 1 = -64$ |
| -1 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | $(1023-1024) \times 1 = -1$ |
| 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(1024-1024) \times 1 = 0$ |
| +120 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | $(1144-1024) \times 1 = 120$ |
| +768 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(1792-1024) \times 1 = 768$ |
| +480* | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | $(1504-1024) \times 2 = 960$ |
| +512* | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(1536-1024) \times 2 = 1024$ |
| +896* | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $(1920-1024) \times 2 = 1792$ |
| +1023 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | $(2047-1024) \times 2 = 2045$ |

^{*} indicates that bit #11 (MSB:Gain Tab Bit) has been set

APPENDIX 1

DESCRIPTION OF RMDU MODULES USED IN FLIGHT TEST

AMX card:

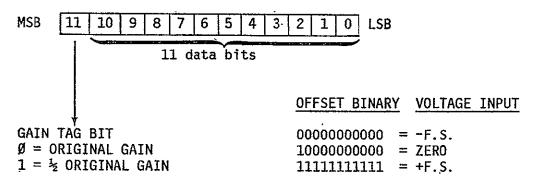
provides 33 addressable low level analog multiplexed channels, one channel of which is devoted to a precision voltage divider providing a 7.3237 mv signal useful for calibration purposes.

PSF card:

provides four independent 4-pole active filter, preamplifiers per card. Dryden's were designed as 50 Hz cutoff. low pass Butterworth filters with gains of 1, 2, and 400.

ADP-M module: the analog data processing module, the heart of the analog processing portion of the RMDU, consists of a gain programmable amplifier, the autoranging circuitry, and the analog to digital (A/D) converter. The amplifier for the Dryden ADP-M has eight programmable gains (1,2,3,10,50,100,400, and 1000). The autoranging section samples the output of the gain programmable amplifier and automatically reduces the gain to ½ of its original value when the output exceeds approximately ±90% of full scale. Upon autoranging, a bit is appended to the most significant portion of the data word (see diagram below). The A/D converter portion of the ADP-M is an eleven-bit bipolar successive approximation converter with a resolution of 5 mv/count (thus giving an overall voltage range to the A/D converter of ±5.115 volts). Dryden's ADP-M is configured for offset binary output coding to remain compatible with the Center's existing ground station capabilities.

ADP-M OUTPUT WORD FORMAT:



The eight programmable gains give an overall resolution and full scale values as follows:

| GAIN | RESOLUTION | FULL SCALE VOLTAGE INPUT | | | | | | | |
|------|-------------------------------|------------------------------|--|--|--|--|--|--|--|
| 1 | 5mv/count * 10 mv/count | ±5.1150 Volts ±10.2300 Volts | | | | | | | |
| 2 | 2½mv/count * 5 mv/count | ±2.5575 Volts ±5.1150 Volts | | | | | | | |
| 3 | 1-2/3mv/count * 3-1/3mv/count | ±1.7050 Volts ±3.4100 Volts | | | | | | | |
| 10 | 500µv/count * 1 mv/count | ±0.5115 Volts ±1.023 Volts | | | | | | | |
| 50 | 100μv/count * 200μv/count | ±0.1023 Volts ±.2046 Volts | | | | | | | |
| 100 | 50μν/count * 100μν/count | ±51.150 mv ±.10230 Volts | | | | | | | |
| 400 | 12 2 v/count * 25 v/count | ±12.789 mv ±25.5750 mv | | | | | | | |
| 1000 | 5μν/count * 10μν/count | ±5.115 mv ±10.2300 mv | | | | | | | |

^{*} indicates autoranged values

SAT-M module:

generates all internal and external time base signals, contains the sampling format memory for the data cycle, and formats the 12 bit digital data for transmission recording on an onboard tape recorder, or both. The available output formats are nonreturn to zero level (NRZ-L), nonreturn to zero Mark (NRZ-M) biphase level (Biø-L), biphase mark (Biø-M), and delay modulation mark (DM-M or Miller).

Dryden's SAT-M was configured for NRZ-L format to the RF transmitter, and DM-M format to the onboard tape recorder. The maximum word rate obtained with the SAT-M is 125,000 WPS (1.5 Mbits/sec).

Dryden's was configured for a word rate of 13,888 WPS (167 Kbits/sec) - again keeping compatible with the existing station firmware setup. The sampling format for the data cycle map is stored in erasable programmable read-only memories (EPROM's) located in the SAT-M. The data cycle sampling format memory contains the information that directs the RMDU channel sampling sequence, gain, and sampling rate. The user has a great deal of flexibility in designing the sampling format memory, however, certain limits and constraints should be observed.

Any number of mainframe channels can be specified up to and including 128 (which includes the synchronization words and the subframe identification word). Similarily, any number of subframe channels can be specified (not to exceed 128 unique parameters) as long as the product of the number of subframe columns and the depth of the deepest subframe column does not exceed 256. These constraints are entirely based upon the size of the memory circuits; newer SAT-M modules are available now from the manufacturer which have considerably larger memory circuits. The NASA Dryden sampling format was comprised of 16 words per frame with the deepest subframe channels (see figures in Appendix 2).

APPENDIX 2

DRYDEN'S SAMPLING FORMAT FOR USE IN FLIGHT TEST

| 0 | 1. | 2 | 3 | ь | 5 | 6 | 7 | .8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | |
|--|------------------------------|---|-----|--------|--------------------|--------------------|----------------------|----------------------|------------------------|---------------------|---------------------|--------------------|--------------------|---------------------|-------------------|-----|
| 5YNCH-1 Ø112 ₈ | synch-2 ø27ø ₈ | sf-id 7øøø ₈ | HLC | rrc-r | АМХ 1-5 ХЬОО | GPA-Ø XLOO | AMX * 1-1 Xhoo | AMX 1-10 X1000 | AMX ** 1-1 X1000 | LLC-1 | GPA-Ø X10 | AMX 1–1կ X10 | AMX 1-14 X3 | AMX* 1-22 X2 | AMX 1-23 X2 | . 0 |
| | | SF-ID 7ØØ1 ₈ | | 1 4400 | N400 | GPA-Ø X400 | AMX * 1-2 X400 | | AMX ** 1-2 X1000 | LLC-1 X1000 | GPA-Ø | AMX 1-15 X10 | AMX 1-15 X3 | AMX 1-24 X2 | AMX 1-25 X2 | 1 |
| | | sr-Id 7øø2 ₈ | | | | | AMX 1-3 X400 | AMX 1-26 X1000 | AMX 1-3 X1000 | LLC-1 X1000 | AMX 1-12 X10 | AMX 1-16 X10 | AMX 1-16 X3 | AMX * 1-22 X1 | AMX 1-23 X1 | 2 |
| | SF-ID 7003 ₈ | | | | | лмх 1-4 х400 | AMX 1-27 X1000 | AMX 1-4 X1000 | LLC-1 X1000 | AMX 1-13 X10 | AMX 1-17 X10 | AMX 1-17 X3 | AMX 1-24 X1 | AMX 1-25 X1 | ,3 | |
| | | sf-Id 7øø4 ₈ | | | | | | | | | | | AMX 6-1 X400 | AMX 6-2 X400 | ц | |
| | | SF-ID 7005 Bit Rate = 167 Kbits/sec Word Rate = 13,888 Words/sec No. Bits/Word = 12 Sample Rate: Main Frame Words = 868 Samples/sec 2-Deep Subframe Words = 434 Samples/sec 4-Deep Subframe Words = 217 Samples/sec | | | | | | | | AMX 6-1 X1000 | AMX 6-2 X1000 | 5 | | | | |
| | | | | | | | | | | AMX 1-26 X400 | AMX 127 X400 | 6 | | | | |
| SF-ID 7007 Note: astericks denote minor changes for Fli in that those channels so marked are p | | | | | | | | | or Flights | 179 and | 481 50 H≈ | PSB | LLC-1 | 7 | | |

^{*} overall gain of these channels are same; the gain programmable amplifier is reduced to unity and the remaining gain occurring in the active filter

^{**} overall gain of these channels are reduced from 1000 to 800; the gain programmable amplifier is induced to a gain of 2 with the active filter providing a gain of 100.

| LINE # | PARAMETER | DESCRIPTION | GAIN | SAMPLE RATE (Samples/sec) |
|--------|------------------|---|------|------------------------------|
| 1 | SYNC-1 | Barker Code: 0112) ₈ | - | 868 |
| 2 | SYNC-2 | Barker Code: 0270) ₈ | | 868 |
| 3 | SF-ID Ø | 7000) ₈ | | 108 ¹ 2 |
| 4 | HLC | High Level Calibration | - | 868 |
| 5 | LLC-1 (AMX 1-33) | Low Level Calibration | 400 | 868 |
| 6 | AMX 1-5 | Shorted at RMDU plug | 400 | 868 |
| 7 | GPA-Ø | GPA zero calibration | 400 | 434 |
| 8 | AMX 1-1 | PT1 Driven shield, RMDU excitation | 400 | 217 |
| 9 | AMX 1-10 | Shorted at RMDU plug | 1000 | 217 |
| 10 | AMX 1-1 | PT1 Driven Shield, RMDU excitation | 1000 | 217 |
| 11 | LLC-1(AMX 1-33) | Low level calibration | 1000 | 217 |
| 12 | GPA-Ø | GPA zero calibration | 10 | 217 . |
| 13 | AMX 1-14 | AC.1 Driven shield, RMDU excitation | 10 | 217 |
| 14 | AMX 1-14 | AC.1 Driven shield, RMDU | 3 | 217 |
| 15 | AMX 1-22 | CPT1 Driven shield, RMDU excitation | 2 | 108½ |
| 16 | SF - ID 1 | | _ | 108½ |
| 10 | 31 ID I | 7001) ₈ | _ | 100-2 |
| 17 | AMX 1-2 | PT2 Non-driven shield, RMDU excitation | 400 | 217 |
| 18 | AMX 1-11 | Shorted at RMDU plug | 1000 | 217 |
| 19 | AMX 1-2 | PT2 Non-driven shield, RMDU bias | 1000 | 217 |
| 20 | AMX 1-15 | AC-2 Non-driven shield, RMDU excitation | 10 | 217 |

| LINE # | PARAMETER | DESCRIPTION | GAIN | SAMPLE RATE |
|----------------------|--|--|--------------|--------------------|
| 21 | AMX 1-15 | AC-2 Non-driven shield, RMDU Excitation | 3 | 217 |
| 22 | AMX 1-24 | CPT3 Driven shield External Excitation | 2 | 108½ |
| 23 | AMX 1-25 | CPT4 Non-driven shield, External Excitation | 2 | 108½ |
| 24 | SF-ID 2 | 7002) ₈ PT3 Driven shield | - | $108\frac{1}{2}$ |
| 25 | AMX 1-3 | External Excitation | 400 | 217 |
| 26 27 | AMX 1-26 AMX 1-3 | 2KΩ Driven shield PT3 Driven shield, | 1000 | 217 |
| | | External Excitation | 1000 | 217 |
| 28 | AMX 1-12 | Shorted at RMDU plug | 10 | 217 |
| 29 | AMX 1-16 | AC.3 Driven shield, External Excitation | 10 | 217 |
| 30 | AMX 1-16 | AC.3 Driven shield, External Excitation | 3 | 217 |
| 31 | AMX 1-22 | CPT1 Driven shield, | J | 217 |
| 04 | 7 31 27 da | RMDU excitation | 1 | 108½ |
| 32 | AMX 1-23 | CPT2 Non-driven shield | <u> </u> | |
| | | RMDU excitation | 1 | 108½· |
| 33 | SF-ID 3 | 7003) ₈ | • | $108\frac{1}{2}$ |
| 34 | AMX 1-4 | PT4 Non-driven shield, External excitation | 400 | 217 |
| 35 | AMX 1-27 | Tape recorder tachomete | | , |
| 00 | 731 183 da da d | rape recorder outrome oc | 1000 | 217 |
| 36 | AMX 1-4 | PT4 Non-driven shield, | | |
| | | External Bias | 1000 | 217 |
| 37 | AMX 1-13 | Shorted at RMDU plug | 10 | 217 |
| 38 | AMX 1-17 | Ac4 Non-driven shield, | | |
| | | External Excitation | 10 | 217 |
| 39 | AMX 1-17 | Ac4 Non-driven shield | | |
| | | External Excitation | 3 | 217 |
| 40 | AMX 1-24 | CPT3 Driven shield, | | |
| | | External Excitation | 1 | 108½ |
| 41 | AMX 1-25 | CPT4 Non-driven shield, | | |
| | | External Excitation | 1 | 108½ |
| 42 | SF-ID 4 | 7004) ₈ | - | $108\frac{1}{2}$ |
| 43 | AMX 6-1 | TC-1 Driven shield | 400 | 108½ |
| 44 | AMX 6-2 | TC-2 Non-driven shield | 400 | 108½ |
| 45 | SF-ID 5 | 7005)8 | - | 108½ |
| 46 | AMX 6-1 | TC-1 Driven shield | 1000 | 108 ¹ 2 |
| 4 0 47 | AMX 6-2 | TC-2 Non-driven shield | 1000 | 108½ 108½ |
| 47 48 | SF-ID 6 | TOTA NUMBER SITER | 7000 | 108½ 108½ |
| 48 49 | AMX 1-26 | 7006) ₈ 2KΩ* Driven shield | 400 | 108½ 108½ |
| 43 | ULIV T_TO | ZMI DITIVEIL SHIETU | 700 | 100-2 |

| LINE # | PARAMETER | DESCRIPTION | GAIN | SAMPLE RATE |
|----------|------------------------|--|----------|--------------|
| 50 | AMX 1-27 | Tape Recorder | | |
| 51 | SF-ID 7 | tachometer 7007) ₈ | 400 | 108½ 108½ |
| 52 53 | PSB LLC-1(AMX 1-33) | Power supply BITE Low level calibration | - 100 | 108½ 108½ |

| MEMORY | | | A Code | G Code | Y Code | X Code | C Code | | |
|--|--|--|---|---|---------------------------------------|---------------------------------------|---|--|--|
| ADDRESS | PARAMETER | <u>GAIN</u> | 4 3 2 1 D | 4 3 2 1 D | 3 2 1 D 7 | 321 | $\frac{2}{D}$ | | Octal |
| 0 1 2 3 4 5 | SYNC 1 SYNC 2 SF-ID HLC LLC-1 AMX 1-5 | - - - 400 400 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 0 1 0 0 1 0 1 1 0 0 0 0 0 0 0 0 0 0 1 0 0 0 1 0 | 1 0 0 0 0 0 0 0 0 1 0 1 | 0 0 0 0 0 0 0 0 0 0 1 0 | 0 0 0 0 0 0 | nm nm nm nm nm nsf | 004 240 013 200 340 000 360 000 102 250 102 021 |
| 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 | GPA-Ø AMX 1-1 AMX 1-10 AMX 1-1 LLC-1 GPA-Ø AMX 1-14 AMX 1-22 AMX 1-23 GPA-Ø AMX 1-21 GPA-Ø AMX 1-15 AMX 1-2 LLC-1 GPA-Ø AMX 1-15 AMX 1-25 AMX 1-25 AMX 1-26 AMX 1-3 LLC -1 AMX 1-16 AMX 1-16 AMX 1-16 AMX 1-16 AMX 1-23 AMX 1-23 AMX 1-23 AMX 1-23 | 400 400 1000 1000 1000 10 10 3 2 400 400 1000 1000 1000 1000 1000 1000 | 0 1 0 0 0 1 0 0 1 1 1 0 0 1 0 0 | 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 1 0 1 1 0 0 0 1 1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 0 1 0 1 0 1 0 1 1 0 0 0 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 1 0 1 0 1 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 0 1 0 0 0 1 0 | nsf nsf nsf nsf nsf nsf nsf nsf nsf nsf | 342 001 102 001 101 055 101 001 101 251 345 001 105 105 110 105 111 155 111 162 342 001 102 005 101 061 101 005 101 251 345 001 105 111 110 111 111 165 111 202 102 011 101 205 101 011 101 251 105 105 115 110 115 110 115 112 155 112 162 102 015 |

EPROMS 1 and 2 MAIN FORMAT MEMORY PROGRAM

| MEMORY: | | | | G Y ode Cod | | | C ode | |
|---|---|---|---|---|---------------------------------------|---|---|--|
| ADDRESS | PARAMETER | GAIN | 4 3 2 1 4' | D D | <u> </u> | 212 | $\frac{1}{D}$ | <u>Octal</u> |
| | • | | 7 | 0 7 | , | | 0 | |
| 158 159 160 161 162 163 164 165 166 167 168 169 170 | AMX 1-27 AMX 1-4 LLC-1 AMX 1-13 AMX 1-17 AMX 1-24 AMX 1-25 AMX 6-1 AMX 6-2 AMX 6-1 AMX 6-2 AMX 6-2 AMX 1-26 AMX 1-26 AMX 1-27 | 1000 1000 1000 10 10 3 1 1 400 400 1000 10 | 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 1 0 1 0 0 1 0 1 0 0 1 1 0 0 1 0 1 0 0 1 0 | 0 0 1 1 0 0 0 1 0 0 0 0 1 1 0 1 0 1 0 1 0 0 0 0 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 nsf 1 nsf 1 nsf 1 nsf 1 nsf 1 nsf 0 eof 1 nsf 0 eof 1 nsf 0 eof | 101 211 101 015 101 251 105 101 105 121 110 121 112 165 112 202 222 001 222 006 221 001 221 006 102 205 102 212 |
| 172 | PSB | - | | 0 0 0 0 0 | | | | |
| 173 | LLC-1 | 100 | | 0 1 1 1 0 | | | 1 eoc | 103 253 |
| | | | | | | | → - | |
| | | | EPROM 1 | | | EPROM | 12 E | PROM 1 EPROM 2 |

Note: "C" Code:

nm = next mainframe
nsf = next subframe
eof = end of frame
eoc = end of cycle
A Code = Card Select
G Code = Gain Select
YX Code = Channel Select

EPROMS 1 and 2 MAIN FORMAT MEMORY PROGRAM (CONCLUDED)

| | DATA | A CONTENTS | DATA CONTENTS | | | |
|-------------------|------------------|--|---------------------|------------------|--|--|
| MEMORY ADDRESS | DECIMAL VALUE | BINARY D ₇ D D D D D D ₀ | MEMORY ADDRESS | DECIMAL VALUE | BINARY D ₇ D D D D D D ₀ | |
| 0 | 128 | 10000000 | 40 | 128 | 10000000 | |
| 1 | 129 | 10000001 | 41 | 129 | 10000001 | |
| 2 | 130 | 10000010 | 42 | 130 | 10000010 | |
| 3 4 | 131 132 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | 43 44 | 131 132 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | |
| 5 | 132 | 10000100 | 44 45 | 132 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | |
| 6 | 134 | 100001110 | 46 | 134 | 10000110 | |
| 7 | 135 | 10000111 | 47 | 135. | 10000110 | |
| 8 | 136 | 10001000 | 48 | 166 | 10100110 | |
| 9 | 137 | 10001001 | 49 | 167 | 10100111 | |
| 10 | 138 | 10001010 | 50 | 138 | 10001010 | |
| 11 | 139 | 10001011 | 51 | 139 | 10001011 | |
| 12 | 140 | 10001100 | 52 | 140 | 10001100 | |
| 13 | 141. | 10001101 | 53 | 141 | 10001101 | |
| 14 | 142 | 10001110 | 54 | 142 | 10001110 | |
| 15 16 | 143 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | 55 56 | 143 | 10001111 | |
| 16 17 | 144 145 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | 56 57 | 144 145 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | |
| 18 | 145 | 1001001 | 58 | 168 | 101010001 | |
| 19 | 147 | 10010010 | 59 | 169 | 10101000 | |
| 20 | 128 | 10000000 | 60 | 128 | 10000000 | |
| 21 | 148 | 10010100 | 61 | 148 | 10010100 | |
| 22 | 149 | 10010101 | 62 | 149 | 10010101 | |
| 23 | 150 | 10010110 | 63 | 150 | 10010110 | |
| 24 | 151 | 10010111 | 64 | 151 | 10010111 | |
| 25 | 152 | 10011000 | 65 | 152 | 10011000 | |
| 26 | 153 | 10011001 | 66 | 153 | 10011001 | |
| 27 | 154 | 10011010 | 67 | 154 | 10011010 | |
| 28 29 | 155 156 | $\begin{smallmatrix} 1 & 0 & 0 & 1 & 1 & 0 & 1 & 1 \\ 1 & 0 & 0 & 1 & 1 & 1 & 0 & 0 \end{smallmatrix}$ | 68 60 | 170 | 10101010 10101011 | |
| 30 | 138 | $egin{array}{cccccccccccccccccccccccccccccccccccc$ | 69 70 | 171 138 | $10101011 \\ 10001010$ | |
| 31 | 157 | 10001010 | 70 71 | 157 | 100010101 | |
| 32 | 158 | 10011110 | 72 | 158 | 10011101 | |
| 33 | 159 | 10011111 | 73 | 159 | 10011111 | |
| 34 | 160 | 10100000 | 74 | 160 | 10100000 | |
| 35 | 161 | 10100001 | 75 | 161 | 10100001 | |
| 36 | 162 | 10100010 | 7.6 | 162 | 10100010 | |
| 37 | 163 | 10100011 | 77 | 163 | 10100011 | |
| 38 | 164 | 10100100 | 78 | 172 | 10101100 | |
| 39 | 165 | 10100101 | 79 | 173 | 10101101 | |

SUBFRAME STEERING (EPROM 3) PROGRAM

OVERHEAD WORD LOCATOR (EPROM 4) PROGRAM

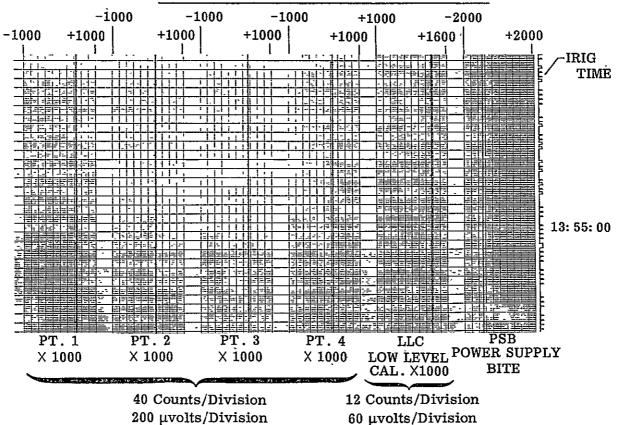
APPENDIX 3a

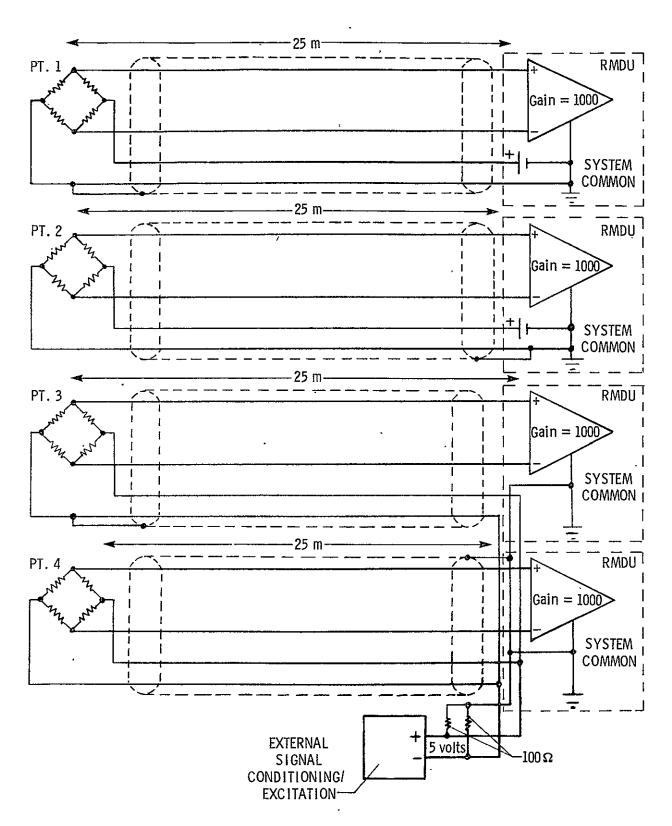
3a. Real Time TM Data and ground station hard copy data for PT. $1 \longrightarrow PT.4$

APPENDIX 3a
GROUND STATION HARD COPY DATA OUTPUT.

| IRIG-B | | AMX 1-2 | <u>AMX 1-3</u> | AMX 1-4 |
|---|---|--|---|---|
| TIME TRACK | X 1000 PT 1 | X 1000 PT. 2 | X 1000 Рт з | X 1000 PT. 4 |
| 13:55:01:222 13:55:01:227 13:55:01:232 13:55:01:232 13:55:01:242 13:55:01:247 13:55:01:257 13:55:01:262 13:55:01:262 13:55:01:267 13:55:01:267 13:55:01:287 13:55:01:287 13:55:01:287 13:55:01:287 13:55:01:287 13:55:01:287 13:55:01:287 13:55:01:282 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 13:55:01:302 | PT. 1 - 420. 420. 420. 420. 425. 425. 419. 419. 427. 427. 427. 421. 421. 421. 424. 424. 423. | 202. 202. 202. 202. 207. 197. 197. 197. 197. 202. 202. 202. 202. 202. 202. 202. 20 | PT. 3 340. 340. 340. 340. 335. 335. 335. 335. 335. 338. 339. 339. 339. 339. 339. 337. 337. 337 | FT . 4 242.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2. |

REAL TIME TELEMETRY STRIP CHART DATA



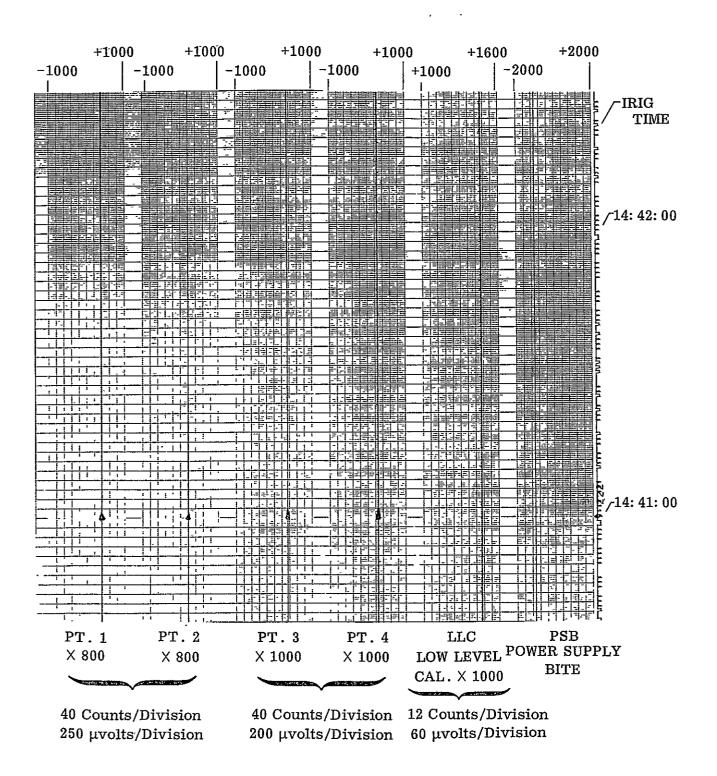


SHIELDING AND EXCITATION CONFIGURATION FOR PT. 1-PT. 4

APPENDIX 3b

3b. Real Time TM Data and ground station hard copy data for PT. $1 \rightarrow$ PT. 4

REAL TIME TELEMETRY STRIP CHART DATA

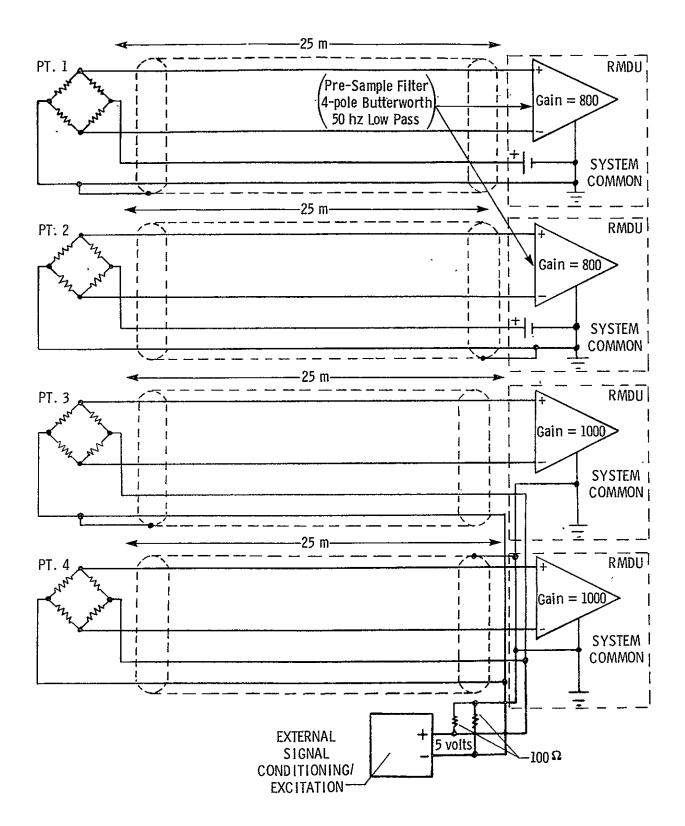


LISTING START TIME: 00:00:00:000

JETSTAR HLT 479 AIFTDS SYSTEM COUNTS

COO!ES:ES:ES : SMIT' DA BALTELL

| IRIG-B | PT. 1 | PT. 2 | PT. 3 | PT. 4 |
|------------------------------|--|--|---|--|
| TIME TRACK | CH 81 | CH 82 | CH 83 | CH 84 |
| * | A1X800 | A2X800 | A3X1000 | A4X1000 |
| 14:41:00:067 | 195. | - 376. 376. | 3945. 339. 339. 339. 339. 341. 341. | 250. 252. 252. 252. 252. 253. 253. |
| 14:41:00:072 | 195. | 376. | 339. | Z52. |
| 14:41:00:082 | 195. | 375. 376. | 333. | 252. 252 |
| 14:41:00:087 | 195. | 376. | 339. | 252. |
| 14:41:00:092 14:41:00:097 | 195. | 376. | 341. | 253. |
| 14:41:00:402 | 195. | 376. | 341. | 253. |
| 14:41:00:107 | 195. | 376. | 341. | 253. |
| 14:41:00:112 | 195. | 375. 376. 376. 376. 376. 377. | 341. | 253. 2550. 2550. 2550. 2550. 25444. 2444. 2447. |
| 14:41:00:117 | 173. | 377 | 344. 344. | 250. |
| 14:41:00:122 14:41:00:127 | 195. | 377. 377. 377. | 344. | 250. |
| 14:41:00:132 | 195. | 377. | 344. 344. 344. | 250. |
| 14:41:00:137 | 195. | 376. | 344. | 252. |
| 14:41:00:142 | 195. | 376. | 344. | 252. |
| 14:41:00:447 | 195. | 376. | 344. 344. | 255- |
| 14:41:00:152 | 196 | 376 | 343 | 244 |
| 14:41:00:157 14:41:00:162 | 195. | 376. 376. 376. 376. 376. 376. 376. 376. | 343 343. 343. | 244 |
| 14:41:00:167 | 195. | 576. | 343. | 244 |
| 14:41:00:172 | 195. | 376. | <u>343</u> . | 244. |
| 14:41:00:177 | 195. | 376. | 343. 345. 345. | 247. |
| 14:41:00:182 | 195. | 376. 276 | 345. | 247. 247. 247. 252. 252. 252. 252. |
| 14:41:00:187 | 195 | 376. 376. 376. 376. | 345. | 247. |
| 14:41:00:192 14:41:00:197 | 196. | 376. | 339. | ž52. |
| 14:41:00:202 | 193 | 276. | 345. 345. 325. 339. 339. 339. 342. | 252. |
| 14:41:00:207 | 196. | 376. | 335. | 252. |
| 14:41:00(212 | 196. | 376. | 335. 242 | ಜಿ52. 326 |
| 14:41:00:217 | 195. | 376. 376 | 342 | 240. 249 |
| 14:41:00(222 14:41:00(227 | 195. | 376 | 342: | 248. |
| 14:41:00:232 | ĩ95. | 376. | 342. | 248. |
| 14:41:00:237 | 19 <u>5</u> . | <u>376</u> . | 342. 342. 342. 344. | 256. |
| 14:41:00:242 | 195. | 676. 376. 376. 376. 376. 376. 376. 376. | 344. 944 | 2488 2488 2456 25677779 257779 |
| 14:41:00(247 | 1 515. | 375. | 344. 344. 344. 344. | 25b. |
| 14:41:00:252 14:41:00:257 | 195. | 376. | 344. | 257. |
| 14:41:00(25) | 195. | ଉଁବରି | 344. | 257. |
| 14:41:00(267 | 195. | 376. 377. 377. | 34 <u>4</u> 1. | 257. |
| 14:41:00:277 | L25. | 377. | 345. | 849. |
| 14:41:00:282 | 195. | 377. coro | 340. | 249. |
| 14:41:00(287 | (98- 195 | 372 | 344. 345. 345. 345. 345. 345. | 249. 249 |
| 14:41:00(292 14:41:00(297 | 195. | 377. | 344. | 25A. |
| 14:41:00:302 | 5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5. | 3777. 377. 377. 377. 377. 377. 377 | نا۱ ۴. | 249. 249. 256. 256. |
| 14:41:00:307 | 195. | 377. | 344. | 256. 256. |
| 14:41:00:1312 | 195. | 377 | 344. | 255. |
| 14:41:00:817 | 195. | 376 376. | 340. 340. | 235. |
| 14:41:00:822 | ເນວ. | arn. | J40. | 236. |



SHIELDING AND EXCITATION CONFIGURATION FOR PT. $1 \rightarrow PT$. 4

PT.1 AND PT.2 (From Flight 439 - Unfiltered Gain = 1000)

PT.1 Gain = 1000 Unfiltered

Median value \overline{X} = 374.00 Counts Mean value \overline{X} = 374.44 Counts Maximum value = 383.00 Counts Minimum value = 367.00 Counts RMS deviation σ = 2.89 Counts

PT.2 Gain = 1000 Unfiltered

Median value \overline{X} = 158.00 Counts Mean value \overline{X} = 163.74 Counts Maximum value = 256.00 Counts Minimum value = 85.00 Counts RMS deviation σ = 54.32 Counts

PT.1 AND PT.2 GAIN = 800 FILTERED (From Flight #479)

PT.1 Gain = 800 Filtered

Median value = 376.00 Counts Mean value = 376.33 Counts Maximum value = 377.00 Counts Minimum value = 376.00 Counts RMS deviation = 0.47 Counts

PT.2 Gain = 800 Filtered

APPENDIX 3c

3c. Internal precision voltage response for gains of 400 and 1000

PRECISION VOLTAGE CHANNELS: (From Flight #481)

Low Level Calibration (7.3237 mv) at Gain = 1000:

```
Median value = 1458.00 Counts

Mean value X = 1457.89 Counts

Maximum value = 1460.00 Counts

Minimum value = 1454.00 Counts

RMS deviation \sigma = 1.15 Counts
```

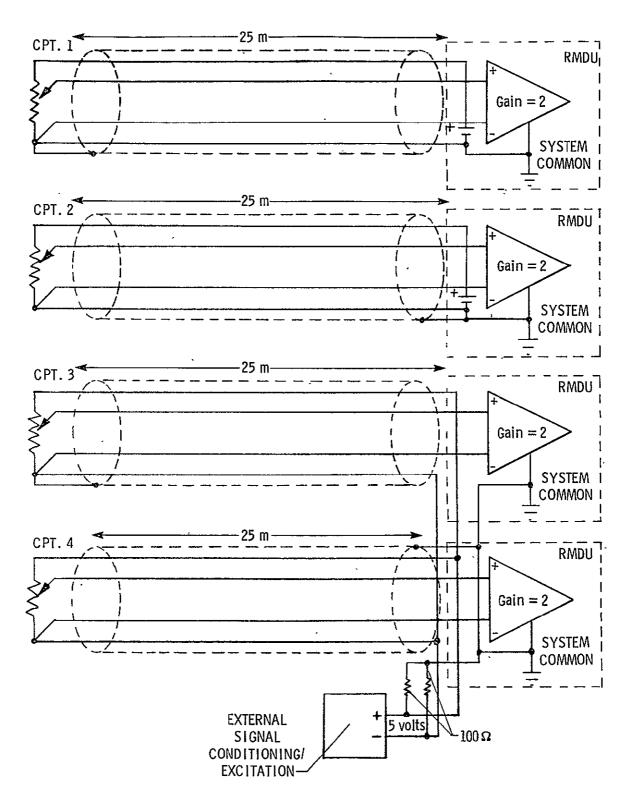
Shorted Channel Response at Gain = 400:

Gain Programmable Amplifier's Zero Response (GPA-Ø) at Gain = 400:

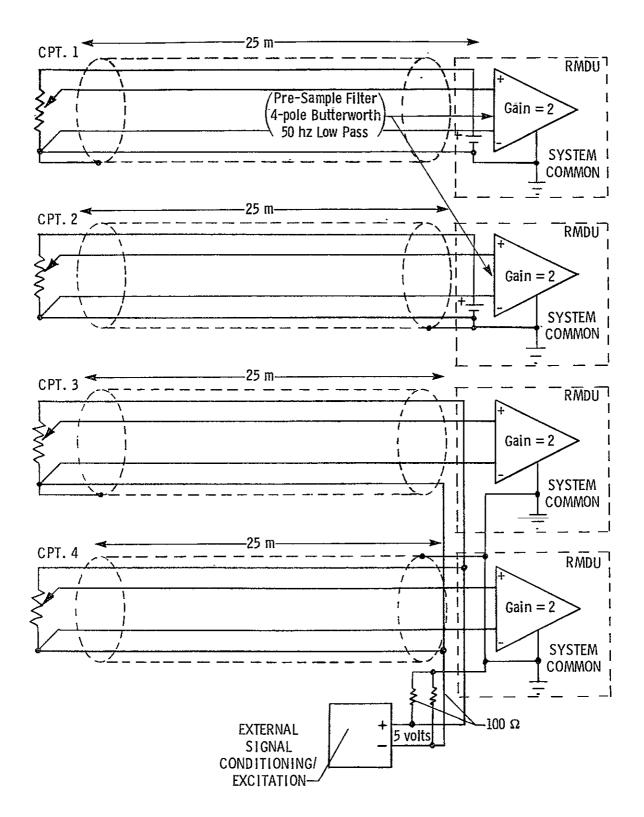
NOTE: For Gains of 1000 each Count = 5μ volts For Gains of 400 each Count = 12μ volts

APPENDIX 3d

3d. Strip chart and ground station hard copy data for CPT1→CPT4 showing shielding, excitation, and pre-sample filter response.

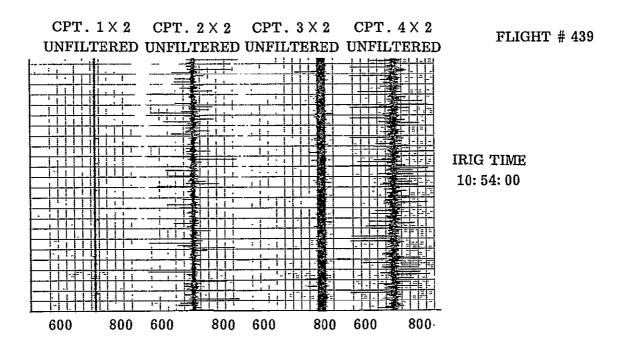


SHIELDING AND EXCITATION FOR CPT. 1-CPT. 4; FLIGHT #439

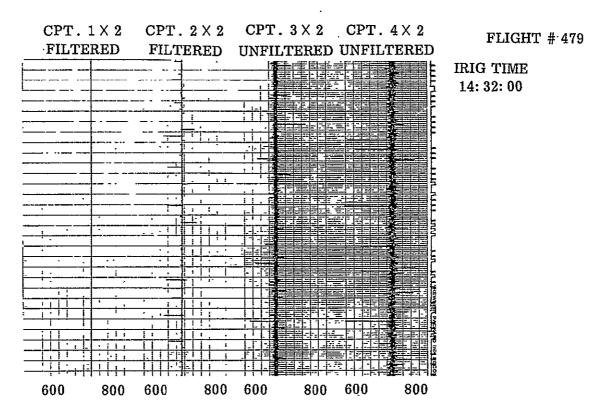


SHIELDING AND EXCITATION - FILTERING FOR CPT. 1-CPT. 4; FLIGHT #479

REAL TIME STRIP CHART TELEMETRY DATA FOR CPT. 1—CPT. 4: FILTERED vs. UNFILTERED



Note: For gain = 2 each division represents 4 counts or 10 mvolts.



LISTING START TIME: 00:00:00:000

LISTING END'TIME: 23:23:23:000

PAGE 2

| JETSTAR FLT | 4 9 | 9 AIFTDS | SYSTEM | COUNTS |
|-------------|-----|----------|--------|--------|

| TIME | | | | JETS: | TAR HLT 4 9 | 9 AIFTDS S | YSTEM COUNT | 15 | | | |
|--|--|-----|--|--|--|--------------|--------------|----------------|--|-----|----------|
| 10 15 10 10 11 12 12 12 12 12 | TIME | | | | | | | CH134 A24X1 | CH144 A25X1 | | |
| 10:54:00:648 709. 701. 775. 705. 354. 352. 392. 354. 1. 0. 10:54:00:653 709. 701. 775. 705. 354. 352. 392. 354. 1. 0. 10:54:00:658 709. 701. 775. 705. 354. 352. 392. 354. 1. 0. | 10:54:00:413 10:54:00:413 10:54:00:428 10:54:00:428 10:54:00:433 10:54:00:443 10:54:00:443 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:453 10:54:00:543 10:54:00:563 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 10:54:00:553 | A22 | AZ 711. 7111. 7111. 7111. 7111. 7111. 7111. 7111. 7111. 7111. 699. 6999. 6999. 6999. 6999. 6999. 6999. 7055. 7055. 7056. 710. 710. 710. 70000. 7000. 7000. 7000. 7000. 7000. 7000. 7000. 7000. 7000. 7000. 7 | A24X2 78807772 | A25X 696. 696. 696. 696. 696. 696. 696. 710. | X | XX | A2 3990 | X 999999999999999999999999999999999999 | A12 | 0 |
| | | | | | | 354. 354. | 352. 352. | | | | ø. ø. |

CPT. 1 CPT. 2 CPT. 3 CPT. 4 CPT. 1 CPT. 2 CPT. 3 CPT. 4 SHORTED SHORTED X 2 X 2 X 2 X 1 X 1 X 1 X 1 CHANNEL CHANNEL X 1 X 1

LISTING END TIME: 23:23:23:000

LISTING START TIME: 00:00:00:000.

| | | | JETS. | TAR ITLT 43 | 9 AIFTDS S | YSTEK COUN | rs | | | |
|--|---|----------------|---|--|--|---------------------------------------|----------------|----------------|---|---|
| TIME | ICH131 IA22X2 | CH141 A23X2 | CH132 A24X2 | CH142 A25X2 | ICH123 IA22X1 | CHI 43 A23X1 | CH134 A24X1 | Ch144 A25X1 | ICH103 A12X10 A | CH104 13X10 |
| 10:54:00:163 10:54:00:163 10:54:00:173 10:54:00:1173 10:54:00:1183 10:54:00:1183 10:54:00:1183 10:54:00:1283 10:54:00:203 10:54:00:203 10:54:00:203 10:54:00:203 10:54:00:228 10:54:00:228 10:54:00:228 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 10:54:00:288 | 711. 7111. 7111. 7111. 7111. 7111. 7111. 7111. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7114. 7116. | 2022 | 774. 774. 7774. 7774. 7781. 7781. 781. 781. 781. 781. 782. 782. 762. 762. 762. 762. 762. 762. 762. 76 | 687.700.7000.7000.7000.7000.7000.7000.70 | 55555544444444444444444444444444444444 | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 33 | 4 | 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1 | HO HO S THE STATE OF THE STATE |
| | OI I . I | OTT. 7 | OTT. 9 | ₩ | ~ I I | \cup 11.4 | OT I. 9 | OF A. 4 | OUCUTED | DITOT |

ORTED X 1 X 1 X 1 X 2 X 2 X 2 CHANNEL CHANNEL X 1 X 1

LISTING START TIME: 00:00:00:000

LISTING END TIME: 23:23:23:000

| | | | JETST | AR MLT 479 | AIFTDS SY | STEM COUNTS | 3 | | | |
|---|--|--|----------------|--|--|---|----------------|---|--------------------------------------|-----------------|
| TIME | ICH131 IA22X2 | CH141 A23X2 | CH132 A24X2 | CH142 A25X2 | ICH133 IA22X1 | CH143 A23X1 | CH134 A24X1 | CH144 A25X1 | ICH103 A12X10 | CH104 A13X10 |
| 14:32:00:842 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:852 14:32:00:857 14:32:00:857 14:32:00:407 | 77777777777777777777777777777777777777 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 667722 | 7777777155.5.5.5.6.6.6.6.6.6.6.9.9.9.9.9.5.5.5.5 | 357. 357. 357. 357. 357. 357. 357. 357. | \$4666666666666666666666666666666666666 | 366.6 | 9999. 966993333333377777777666666666633333333888335555555555 | - 1. - 1. - 1. - 1. - 1. | |

CPT. 1 CPT. 2 CPT. 3 CPT. 4 CPT. 1 CPT. 2 CPT. 3 CPT. 4 SHORTED SHORTED X 2 X 2 X 2 X 1 X 1 X 1 X 1 CHANNEL CHANNEL FILTERED FILTERED FILTERED FILTERED X 1 X 1

LISTING END'TIME: 23:23:23:000

PAGE 5

| LISTING START | TIME: 00:0 | 900:00:00 | | | | | | | LI | STING END: |
|--|--|----------------|---|--|---|--|---|--|------------------------------|---|
| | | | JETS: | TAR IILT 479 | AIFTDS S | STEM COUNT | rs | | | |
| TIME | ICH131 IAZZXZ | CH141 A23X2 | CH132 A24X2 | CH142 A25X2 | ICH133 IA22X1 | CH143 A23X1 | CH134 A24X1 | CH144 A25X1 | TICH103 A12X10 | CH104 A13X10 |
| 14:32:00:607 14:32:00:77 14:32:00:77 14:32:00:77 14:32:00:77 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 14:32:00:807 | 716. 716. 716. 716. 716. 716. 716. 716. | | 666772222222222222222222222222222222222 | 7166.6.6.77144.4.4.777777777777777777777 | 357. 3577. 3577. 35777. 355777. 3557777. 3557777. 35577777. 3557777777777 | ************************************** | 148888888888999999999999999999999999999 | +1NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN | - Î. - 1. - 1. - 1. | 111111111111111111111111111111111111111 |

CPT. 1 CPT. 2 CPT. 3 CPT. 4 CPT. 1 CPT. 2 CPT. 3 CPT. 4 SHORTED SHORTED X 2 X 2 X 2 X 1 X 1 X 1 X 1 CHANNEL CHANNEL FILTERED FILTERED FILTERED X 1 X 1

UNFILTERED DATA FROM CPT.1 AND CPT.2 (From Flight #439)

CPT.1 Gain = 2 Unfiltered

Median value \overline{X} = 712.00 Counts Mean value \overline{X} = 411.42 Counts Maximum value = 714.00 Counts Minimum value = 709.00 Counts RMS deviation σ = 1.34 Counts

CPT.1 Gain = 2 Unfilitered

FILTERED DATA FROM CPT.1 AND CPT.2 (From Flight #479)

CPT.1 Gain = 2 Filtered

Median value = 716.00 Counts Mean value = 716.00 Counts Maximum value = 716.00 Counts Minimum value = 716.00 Counts RMS deviation σ = 0.00 Counts

CPT.2 Gain = 2 Filtered

Median value = 692.00 Counts Mean value = 692.32 Counts Maximum value = 694.00 Counts Minimum value = 692.00 Counts RMS deviation σ = 0.61 Counts

| 1. Report No. NASA TM-72867 | 2 Government Access | ion No | 3. Recîpient's Catalog | No | | | | |
|---|--------------------------|---|--|------------------|--|--|--|--|
| 4 Title and Subtitle | | 730 | 5. Report Date July 1979 | | | | | |
| AIFTDS STAND-ALONE RMDU F | LIGHT TEST REPO | RT | 6 Performing Organization Code H-1099 | | | | | |
| 7. Author(s) | | | 8. Performing Organiza | ation Report No. | | | | |
| Douglass O. Wilner | | ļ., | 10. Work Unit No | | | | | |
| 9 Performing Organization Name and Address | | 992-03-01 | | | | | | |
| NASA Dryden Flight Research (P.O. Box 273 Edwards, California 93523 | | 11. Contract or Grant No | | | | | | |
| 12. Sponsoring Agency Name and Address | | | 13. Type of Report an | d Period Covered | | | | |
| National Aeronautics and Space | Administration | | Technical Memorandum 14. Sponsoring Agency Code | | | | | |
| Washington, D.C. 20546 | | | 14. Sponsoring Agency | Code | | | | |
| 15 Supplementary Notes | | | | | | | | |
| A stand-alone RMDU (remote multiplexer/digitizer unit) was subjected to a flight test environment. This flight test provided a mechanism for the Measurement Engineering Branch to closely scrutinize the response of the RMDU and its associated instrumentation circuitry during an actual flight test. Various instrumentation and shielding schemes were employed during the flight test with the data analysis presented in this report. | | | | | | | | |
| 17. Key Words (Suggested by Author(s)) Airborne Integrated Flight Test Data System (AIFTDS) Pulse Code Modulation Data Acquisition Shielding Instrumentation Techniques | | 18. Distribution Statement Unclassified | | 06 | | | | |
| 19 Security Classif. (of this report) | 20. Security Classif. (c | <u> </u> | 21 No. of Pages | 22. Price* | | | | |
| Unclassified | Unclassified | | 63 | \$4.25 | | | | |

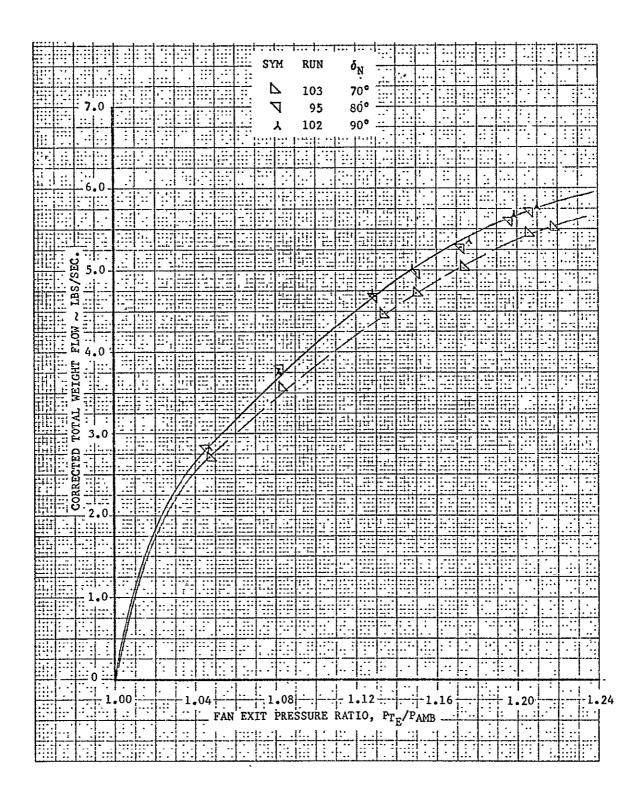


Figure C-6. Fan Calibration, Fan No. 5, Ser. No. 421 (Continued)

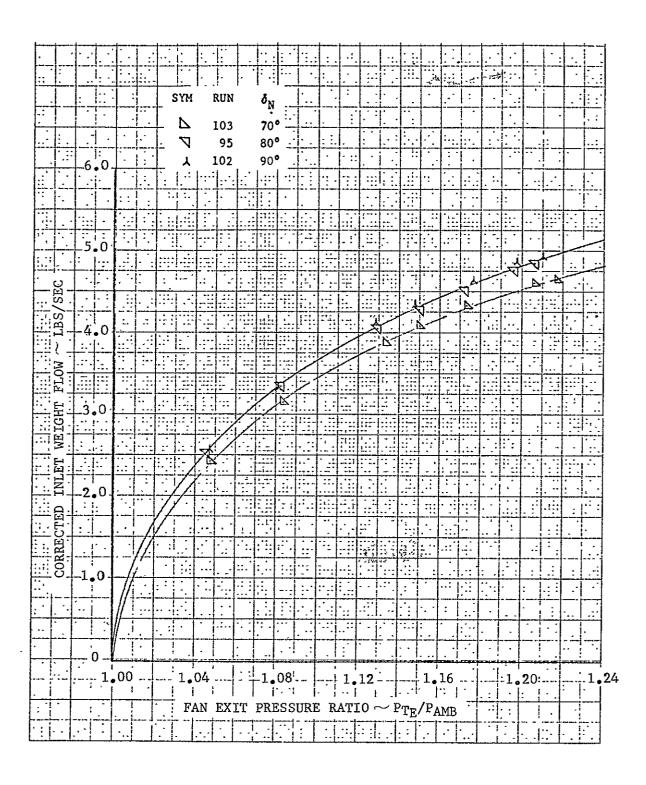


Figure C-6. Fan Calibration, Fan No. 5, Ser. No. 421 (Concluded)